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PATENT SPECIFICATION



Date of filing Complete Specification Feb. 12, 1953

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No. 5302/52.

Complete Specification Published Aug. 31, 1955.

Index at acceptance :- Class 32, A2A.

COMPLETE SPECIFICATION

Improvements in or relating to the Concentration of Fatty Acids in Aqueous Solution and to the Recovery of said Acids from Aqueous Solutions thereof by Azeotropic Distillation

We, THE BRITISH PETROLEUM COMPANY trope is removed overhead. Operating in this Limiten, previously known as Anglo-Iranian Oil Company Limited), of Britannic House, Finabury Circus, London, E.C.2, a British 5 Joint-Stock Corporation and WILFRED SAMUEL NATHAN and TIMOTHY ARROWSMITH RAYNE, both of the Company's Research Station, Chertsey Road, Sunbury-on-Thames, Middlesex, and both of British Nationality, do hereby 10 declare the invention, for which we pray that a parent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following state-

This invention relates to an improved process for the concentration of farry acids in aqueous solution and for the recovery of fatty acids from aqueous solution in the anhydrous

A process has hitherto been described in which fatty acids in dilute solution are concentrated by liquid/liquid solvent extraction using, as solvent, a mixture containing a hydrocarbon and an aliphatic ketone, there-25 ster distilling the extract, containing fatty said in the presence of a diminished amount of water, to obtain on overhead fraction containing water and solvent, allowing the condensate to separate into two layers and returning the 30 layer containing solvent to the mixture undergoing distillation. It is apparent that the above process requires the use of two separate process units, that is a liquid/liquid solvent extraction unit and a distillation unit, said 85 distillation unit receiving solvent in admixture with a fatty acid solution which has already received a substantial concentration treatment in said solvent extraction unit.

It has now been found that provided the 40 overhead fraction, referred to hereinbefore, is condensed and treated for the recovery of an upper phase, comaining solvent, and said upper phase is recycled to the column head, it is possible to maintain in the upper part of the 45 column sufficient solvent and hydrocarbon to ensure that a ketone/water/hydrocarbon azeomanner it has been found that fatty acid aqueous solutions of any concentration may be treated in economic manner for the removal of 50 water in a single stage distillation operation.

It is an object of the present invention to provide an improved process for the concentration of fatty acids in aqueous solution. It is a further object to provide an improved pro- 55 cess for the recovery of fatty acids, from aqueous solution, in the anhydrous STRIC.

According to the present invention, an squeous solution comprising one or more fatty 60 acids having 1-4 carbon atoms/molecule is fractionally distilled in a distillation column operated in continuous manner in the presence of an aliphatic ketone having 4-7 carbon atoms/molecule and a volatile hydrocarbon, 65 whereby an overhead product is removed comprising said kerone, said volatile hydrocarbon and water, thereafter condensing said overhead fraction, separating the condensed fraction into a lower phase comprising water and 70 ketone and an upper phase comprising ketone and hydrocarbon, recycling said upper phase to the head of said column, distilling said lower phase for the concentration of ketone contained therein and blending the recovered 75 ketone with the aqueous solution of fatty acid fed to the distillation column.

Preferred ketones are butanone, 2-methylbutanone-3, pentanone-2 and pentanone-3. Other suitable ketones are the hexanones and 80

Preferably volatile hydrocarbons employed which boil within the range 0-10° C. below the boiling point of the ketone.

When using butanone, the preferred vola- 85 tile hydrocarbons are benzene and cyclo-hezane. When using a C, ketone, the preferred volatile hydrocarbons are methylcyclohexane and n-heptane. Other preferred hydrocarbons for use with C, or C, ketones are 90 paraffin hydrocarbons or mixtures of paraffin hydrocarbons boiling over a range of not more

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Price 25p

than 10° C. and preferably over a range of not more than 5° C.

In accordance with preferred procedure, hexanones and higher ketones are not employed for the treatment of solutions of formic acid or acetic acid-or fatty acid solutions comprising formic and/or acetic acid. In the presence of formic acid, pentanones are not usually employed, 2-buttonone being the pre-10 ferred ketone. However, if pentanones or hexanones are used for the treatment of acid mixtures containing formic and acetic acids and higher molecular weight acids (although they boil at about the same temperatures as the 15 anhydrous formic and acetic acids) it is desirable to allow traces of water to penetrate below the level of the entrainer in the stripping section of the column. The bottom few plates of the column are then employed in stripping 20 this residual trace of water by straight distillation.

By the process of the present invention there is provided means for effecting an attention water removal process with efficient recovery 25 of the ketone therein employed.

The process of the invention is illustrated but in no way limited with reference to the drawing accompanying the provisional specification.

With reference to said drawing:-Aqueous fatty scids are introduced by line (9) and are passed together with recycled aqueous ketone, introduced by line (10), through preheater (1) to drying column (2). Dried acids are removed from the column base by line (11) and divided into two streams. One stream is circulated through rebuiler (3) and the other passes through a cooler (4) and is then withdrawn from the system by line (12). 40 The distillate is removed by line (13) and passes through condenser (5) into separator (6), the upper kerone and hydrocarbon layer being returned to the column head by (14). The lower, aqueous phase passes 45 by line (15) to stripping column (7) to which steam is fed by line (19) An azestropic mixture of betone and water is removed overhead from column (7) by line (16) and is passed to condenser (8). Part of the 50 condensed aqueous ketmee is returned as reflux to calasim (7) by line (17) and part re-cycled by line (10) to the feed of agreems sends extering the system. The stripped water from the base of column (7) is run to waste by line

The invention is further illustrated but it no way limited by the following examples.

Brander I

Operating in the massive described with 60 reference to the drawing accompanying the provisional specification and using butaning (methyl ethyl ketone) and syclabranic as the ketone and volatile hydrocarbon respectively, an aqueous acid mixture of the following com-

position was fed at 100 ml per hour, to a fractionating column of 40 theoretical plates with feed admitted at the 20 theoretical plate level.

COMPOSITION OF FEED Formic acid 70 grams					
Acetic Acid Water			63 0	Brams Brams	70
Column temp	 eratures	were:	300	grams	
Top			- 66	.5° C.	
Feed level			- 10	χο° C.	
Base				5° C.	75
Aqueous phase v	VBS remo	wed fr	om the	eparator	
(6) at 34 ml./hr. of butanone in s was stripped fro	and cot plusion. on the v	ntained This waste v	9.0% b dissolve water in	y weight d ketone column	٠
(7) as a ketome/	water a	zeotroi	e (b.p.	73° C.)	80
which was retu	ened to	the s	vstem 1	with the	
aqueous acids fe	ad to ep	e mair	colum	n. The	
waste water was	dans ne	titral a	nd cont	ained no	
detectable quan	enty of	FORM	acid (or acetic	
					85
- The dried acid contained:					
Water - 0.32 % by weight					
The overhead product contained (as % by					
weight thereof):	procus	r earm	series fa	#7o. ery	90
weeken mercury.		. ·		· · · · · · · · · · · · · · · · · · ·	ขบ
Upper phase Lower phase					
Butanone	32	7.3	Ð	78	•
Cycloherane	53		0.	17	
Water	2.	55	5.	25	•

What we claim is:---

 A process for the concentration of fatty acids in aqueous solution which comprises fractionally distilling an aqueous solution compris- 95 ing one or more fatty acids having 1-4 carbon atoms/molecule in a distillation column opersted in continuous manner in the presence of an alighatic ketone baving 4-7 carbon aroms molecule and a volatile hydrocarbon, whereby 100 an overhead product is removed comprising said become, said volatile hydrocarbon and water, thereafter condensing said overhead fraction, separating the condensed fraction into a lower phase comprising water and ketone and 105 an upper phase comprising ketone and hydrocarbon, secycling said upper phase to the head of said cohumn, distilling said lower phase for the concentration of ketone contained therein and blending the recovered ketone with the 110 expresses solution of fatty said fed to the distillation column.

2. A process according to Claim 1 in which the volatile hydrocarbon boils at the boiling point of the kecome or not more than 10° C 116 below said boiling point.

3. A process according to Claim 1 or 2 in which the kenne is bureneste.

4. A process according to Claim 3 in which the volatile hydrocarbon is benzene.

5. A process according to Claim 3 in which the volatile hydrocarbon is cyclohexane.

the ketone has five carbon atoms/molecule.

7. A process according to Claim 6 in which the volatile hydrocarbon is methylcyclohexane. 8. A process according to Claim 6 in which

the volatile hydrocarbon is normal heptane. 9. A process according to any of the preceding claims in which the ketone is a C, or C, ketone and in which the volatile hydrocarbon 10 is a paraffin hydrocarbon or in which there is

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6. A process according to Claim 1 in which used a mixture of paraffin hydrocarbons boiling over a range of not more than 5° C.

10. A process for the concentration of fatty acids in aqueous solution substantially as hereinbefore described with reference to the draw- 15 ing accompanying the provisional specification.

11. Fatty acids wherever concentrated by a process as claimed in any of claims 1-10.

T. MACDÒNALD, For the Applicants.

PROVISIONAL SPECIFICATION

Improvements in or relating to the Concentration of Fatty Acids in Aqueous Solution and to the Recovery of said Acids from Aqueous Solutions thereof by Azeotropic Distillation

Anglo-Iranian OldCOMPANY. 20 LIMITED, of Britannic House, Finsbury Circus, London, B.C.2, a British joint-stock Corporation and WILFRED SAMUEL NATHAN and TIMOTHY ARROWSMITH RAYNE, of the sforesaid Company's address, and both of British 25 nationality, do hereby declare this invention to be described in the following statement:

This invention relates to an improved process for the concentration of fatty acids in aqueous solution and for the recovery of fatty 30 acids from aqueous solution in the anhydrous

It is known that organic acids may be recovered from dilute squeous solutions by distillation in the presence of an entrainer to 35 remove water overhead. A process has been described in French Specification No. 856,562 for the removal of water from aqueous acetic acid in which ethyl acetate is employed as the entrainer, a quantity of low boiling hydro-40 carbon being maintained in the upper part of the distillation column while distillation is in rogress. It has been found that ethyl acetate is limited, in its application to the dehydration of fatty acids, to the treatment of acetic acid 45 since, in the presence of other members of the series, an ester-interchange reaction takes place which leads to loss of the entrainer.

It is an object of the present invention to provide an improved process for the concen-50 tration of farty acids in aqueous solution. It is a further object to provide an improved process for the recovery of fatty acids, from aqueous solution, in the anhydrous state.

According to the present invention,

55 aqueous solution comprising one or more fatty acids is fractionally distilled in the presence of an aliphatic ketone whereby an azeotrope comprising the ketone and water is removed as an overhead fraction.

Preferred ketones are 2-buttanone, pentanones and hexanones. When these ketones are employed it has been found very advantageous to maintain, in the distillation column, a quantity of a volatile hydrocarbon, whereby a 85 kenne/water/hydrocarbon azeotrope removed overhead. Preferably volatile hydro-

carbons are employed which boil with 10° C. of the boiling point of the ketone.

When using 2-butanone, the preferred volstile hydrocarbons are benzene, cyclohexane, 70 paraffin hydrocarbons and mixtures of paraffin hydrocarbons boiling over a narrow range of not more than 10° C. but preferably 5° C.

Hexanones and higher ketones are not generally suitable for the treatment of solutions of 75 formic acid or acetic acid or fatty acid solutions comprising formic and/or acetic In. the presence αŤ formic pentanones are not generally suit-

able, 2-butanone being the preferred ketone.

The overhead product obtained by distillation when operation in the absence of a volatile hydrocarbon may be separated into an upper layer consisting essentially of the ketone, which is recycled for treating further quan- 85 tities of feedstock, and a lower aqueous layer containing some kerone. This aqueous layer may be treated by stripping or by solvent extraction for the recovery of the ketone for re-

When operating in the presence of a volatile hydrocarbon, the overhead product, on condensing, forms two phases. The lower, aqueous layer is removed and the upper layer, consisting essentially of the hydrocarbon and ketone 95 and being substantially free of water, is returned to the top of the distillation column.

The process of the invention is particularly suitable for continuous operation.

The process of the invention is illustrated 100 but in no way limited by the accompanying Figure

With reference to said figure:-Aqueous fatty acids are introduced by line (9) and are passed together with recycled 106 ketone, introduced by line (10), through preheater (1) to drying column (2). Dried acids are removed from the column base by line (11) and divided into two streams. One stream is circulated through reboiler (3) and the other 110 passes through a cooler (4) and is then withdrawn from the system by line (12). The distillate is removed by line (13) and passes through condenser (5) into separator (6), the

upper ketone layer being returned to the column head by line (14). The lower, aqueous phase passes by line (15) to stripping column (7) to which steam is fed by line (19). Ketone 5 is removed overhead from column (7) by line (16) and is passed to condenser (8). Part of the condensed ketone is returned as reflux to column (7) by line (17) and part recycled by line (10) to the feed of aqueous acids entering 10 the system. The stripped water from the base of column (7) is run to waste by line (18).

The invention is further illustrated but in

no way limited by the following example.

EXAMPLE

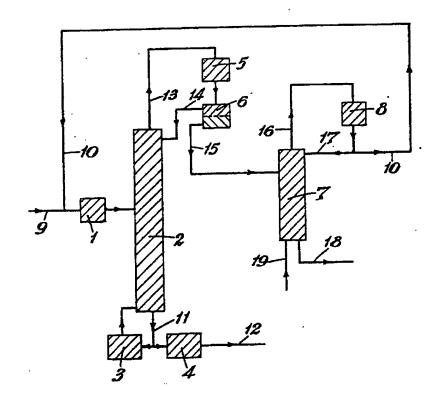
Operating in the manner described with reference to the accompanying figure and using butanone and cycloherane as the kerone and volatile hydrocarbon respectively, an aqueous acid mixture of the following composition was fed to the system at 100 ml. per hour.

COMPOSITION OF FRED Formic acid -70 grams Aceric Acid -630 grams Water 300 grams Aqueous phase was removed from the separator (6) at 34 ml./hr. and contained 9.0% by weight of butanone in solution. This dissolved ketone was stripped from the waste water in column (7) as a ketone/water azeotrope (b.p. 80 73° C.) which was returned to the system with the aqueous acids fed to the main column. The waste water was quite neutral and contained no detectable quantity of formic acid or acetic acid. The water content of the dried acid from 35 the base of column (2) was found to vary between 0.21—0.33% by weight when determined by Fischer Reagent and to contain no detectable quantity of butanone.

T. MacDONALD, For the Applicants.

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735,867 PROVISIONAL SPECIFICATION 1 SHEET This drawing is a reproduction of the Original on a reduced scale.



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